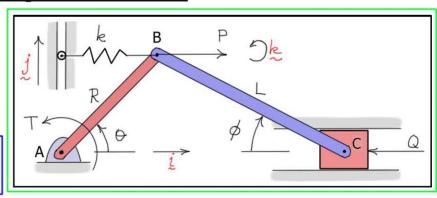
Example #18 – Intermediate Dynamics: Principle of Virtual Work

Active Forces/Torques:

- \circ P, Q, T (neglecting weight forces)
- o spring (unstretched length, ℓ_u)

Find:

 \circ Force Q required to hold the system in equilibrium at some angle θ



Solution: (using θ as the generalized coordinate)

For equilibrium of this system, the *principle of virtual work* states

$$F_{\theta} = (F_{\theta})_{P} + (F_{\theta})_{Q} + (F_{\theta})_{spring} + (F_{\theta})_{T} = 0$$

Here,

$$\begin{split} &(F_{\theta})_{P} = (Pi) \cdot \left(\frac{\partial \underline{v}_{B}}{\partial \dot{\theta}}\right) = (Pi) \cdot \frac{\partial}{\partial \dot{\theta}} \left(R\dot{\theta}(-S_{\theta}i + C_{\theta}j)\right) = (Pi) \cdot \left(R(-S_{\theta}i + C_{\theta}j)\right) = \overline{-PRS_{\theta}} \\ &(F_{\theta})_{spring} = (-f_{sp}i) \cdot \left(\frac{\partial \underline{v}_{B}}{\partial \dot{\theta}}\right) = (-f_{sp}i) \cdot \left(R(-S_{\theta}i + C_{\theta}j)\right) = f_{sp}RS_{\theta} = \overline{k(RC_{\theta} - \ell_{u})RS_{\theta}} \\ &(F_{\theta})_{Q} = (-Qi) \cdot \left(\frac{\partial \underline{v}_{C}}{\partial \dot{\theta}}\right) = (-Qi) \cdot \left[-R\left(S_{\theta} + C_{\theta}S_{\phi}/C_{\phi}\right)i\right] = \overline{QR\left(S_{\theta} + C_{\theta}S_{\phi}/C_{\phi}\right)} \\ &(F_{\theta})_{T} = (Tk) \cdot \left(\frac{\partial \underline{\omega}_{AB}}{\partial \dot{\theta}}\right) = Tk \cdot k = \overline{T} \end{split}$$

Substituting into the principle of virtual work and solving for Q gives

$$F_{\theta} = 0 = -PRS_{\theta} + k(RC_{\theta} - \ell_{u})RS_{\theta} + QR(S_{\theta} + C_{\theta}S_{\phi}/C_{\phi}) + T$$

$$\Rightarrow Q = \frac{PRS_{\theta} - k(RC_{\theta} - \ell_{u})RS_{\theta} - T}{R(S_{\theta} + C_{\theta}S_{\phi}/C_{\phi})}$$

Notes:

- o Pin forces at A, B, and C and normal force at C do not contribute to F_{θ} ("non-active")
- \circ Forces and torques that contribute to F_{θ} are said to be "active"
- o There is only *one equation* associated with the *degree-of-freedom* of the system.
- o The *choice* of generalized coordinate is ours.
- The contribution of the spring could be calculated using potential energy.

$$(F_{\theta})_{spring} = -\frac{\partial V_{sp}}{\partial \theta} = -\frac{\partial}{\partial \theta} \left(\frac{1}{2}ke^{2}\right) = -\frac{1}{2}k\frac{\partial}{\partial \theta} \left(RC_{\theta} - \ell_{u}\right)^{2} = \boxed{k(RC_{\theta} - \ell_{u})RS_{\theta}}$$

Kamman - Intermediate Dynamics - Example #18 - Principle of Virtual Work applied to Slider-Crank Mechanism